



Cost of Capturing CO₂ from Industrial Sources

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11/06/2013



U.S. DEPARTMENT OF
ENERGY

National Energy
Technology Laboratory

Acknowledgments

- **Alex Zoelle (Booz Allen Hamilton)**
- **Steve Herron (Worley Parsons)**
- **Phil Dipietro (NETL)**
- **Mike Matuszewski (NETL)**
- **Kristin Gerdes (NETL)**
- **John Wimer (NETL)**

Outline

- **Objective**
- **Methodology**
- **Study Overview**
- **Key Takeaways**
- **Study Results**

Objective

- **To develop baseline information on the cost of capturing CO₂ from industrial processes for use in enhanced oil recovery (EOR)**
- **To determine which industrial sources could supply CO₂ for EOR at a lower cost than fossil power plants with capture**
- **This information will feed cost-supply curves for an update to an NETL custom version of NEMS**

Methodology

Assumption Overview

- **Base Plant**
- **Capture Plant**
- **Point Sources**
- **CO₂ End Use**
- **Financing**
- **Uncertainties**

Key Assumptions to Consider Base Plant

- **Motivation for capture (i.e. additional revenue or to avoid a penalty) may impact the following:**
 - Extent of capture
 - CO₂ point sources to consider within plant
- **Types of industrial sources to investigate**
 - Is the industry a large emitter of CO₂?
 - Does the source provide a cost effective capture opportunity?
 - Do representative plant sizes provide necessary economies of scale?
 - Determine a cutoff point for CO₂ purity or partial pressure
 - Is the industry located near EOR or CO₂ storage sites?
- **Size of the representative plant**
 - How does assumed plant represent the industrial fleet?
 - Fleet average
 - Next build

Key Assumptions to Consider cont.

Base Plant

- **Is CO₂ being used or vented?**
 - Example: CO₂ used for urea production in an ammonia plant
- **CO₂ point source(s)**
 - CO₂ purity
 - Amount of CO₂ available to be captured
 - Multiple sources within a plant?
 - Will they be combined or utilize separate capture facilities?
 - Concentrations and partial pressures of each source?
 - End use for CO₂
 - EOR
 - Storage
 - Partial pressure of CO₂ in vent stream

Key Assumptions to Consider Capture Plant

- **Will capture plant integrate with Base Plant?**
- **Auxiliary power purchased from grid, utilized from base plant, or produced onsite? Purchase price?**
- **Auxiliary steam source? Associated cost?**
- **Cooling water?**
- **What type of post combustion capture process?**
 - Solvent
 - MDEA, MEA, Selexol, etc.
 - Sorbent
 - Membrane
 - Additional clean-up needed?

Uncertainties to Consider

- **Finance structure**
 - Debt/Equity
 - Cost of debt and equity
 - Economic life
 - Universal or industry specific
- **Capacity Factor of capture plant**
- **Technology maturity**
- **Site specific costs**
- **Sensitivities**

Special Cases to Consider

- **Co-production?**
 - i.e. Ammonia and CO₂ used to make Urea
- **Additional clean-up needed?**
 - Cement may require SCR and FGD before CO₂ removal

Study Overview

- **Industrial processes were limited to domestic plants with flue gas streams containing higher CO₂ concentrations than that of coal-fired power plants (CFPP) (~8-14% CO₂ by volume)**
- **Representative plant sizes were selected for each industry**
 - Average, next built
- **No integration considered between the base plant and the capture plant for all cases**

Case Summary				
Process	Data Source	Greenfield	Retrofit	Retrofit Factor
Ethanol	Literature Review	X	X	1.01
Ammonia	Literature Review	X	X	1.01
Refinery Hydrogen	Literature Review	X	X	1.05
Steel/Iron	Literature Review		X	1.05
Natural Gas Processing	Literature Review	X	X	1.01
Ethylene Oxide	Literature Review	X	X	1.01
Cement	Literature Review	X	X	1.05
Coal-to-Liquids	NETL Study	X		1.01
Gas-to-Liquids	NETL Study	X		1.01

Study Overview Continued

- **Adequate plot plan space for capture and/or compression plant footprint is assumed for all cases**
- **Power purchased at \$59/MWh* for CO₂ compression and other auxiliary loads**
- **Natural gas purchased at \$6.13/MMBtu** for steam generation and all thermal loads**
- **Assumes NOAK cost estimate with +30%/-15% Accuracy**
- **All cases utilize post combustion capture**
- **Capture plants were modeled using the Methyldiethanolamine (MDEA) Acid Gas Removal (AGR) process**
 - MDEA was beneficial due to its sulfur tolerance
 - MDEA appropriate for low pressure requirements compared to Selexol
 - MDEA cost quotes best match for industrial sources capacities versus other amines
- **Breakeven selling price of CO₂ was the metric used to compare results across all cases**

*Purchase price for power based off the cost of electricity (COE) from a NGCC without capture from the NETL Bituminous Baseline Report

**NETL "QGESS: Fuel Prices for Selected Feedstocks in NETL Studies" November 2012

Process Overview

Process	Representative Plant Capacity	Process Vent Stream
Ethanol	50 MMgal/year	Distillation gas
Ammonia	907,000 tonnes/year	Stripping vent
Refinery Hydrogen	59,000 tonnes/year	PSA tail gas
Steel/Iron	2.54 Mt/year	COG PPS COG+BFS
Natural Gas Processing	500 MMscf/d	CO ₂ vent
Ethylene Oxide	364,500 tonnes/year	AGR CO ₂ stream
Cement	992,500 tonnes/year	Kiln Off-gas
Coal-to-Liquids	50,000 bbl/d	AGR CO ₂ streams
Gas-to-Liquids	50,000 bbl/d	AGR CO ₂ stream

Process Distinctions

- **High CO₂ concentration industrial sources**
 - Assumed that vent streams can meet CO₂ pipeline specs* through compression and cooling alone (e.g. $\geq 95\%$ CO₂)
- **Low CO₂ concentration industrial sources**
 - Assumed that vent streams will need to be equipped with both CO₂ capture and compression equipment to meet CO₂ pipeline specs* (e.g. $\geq 95\%$ CO₂)

Financial Assumptions

Financial Parameter	High CO₂ Concentration Cases	Low CO₂ Concentration Cases
Capital Expenditure Period	1 year	3 years
Debt/Equity Ratio	50/50	50/50
Economic Life	30 years	30 years
Interest on Debt	8.0%	8.0%
Return on Equity	20%	20%
Capital Charge Factor (CCF)	15.2%	17.6%

- DCF analysis is done on a current-dollar basis, yielding a "first-year" cost of CO₂ capture.

Results

Key Takeaways

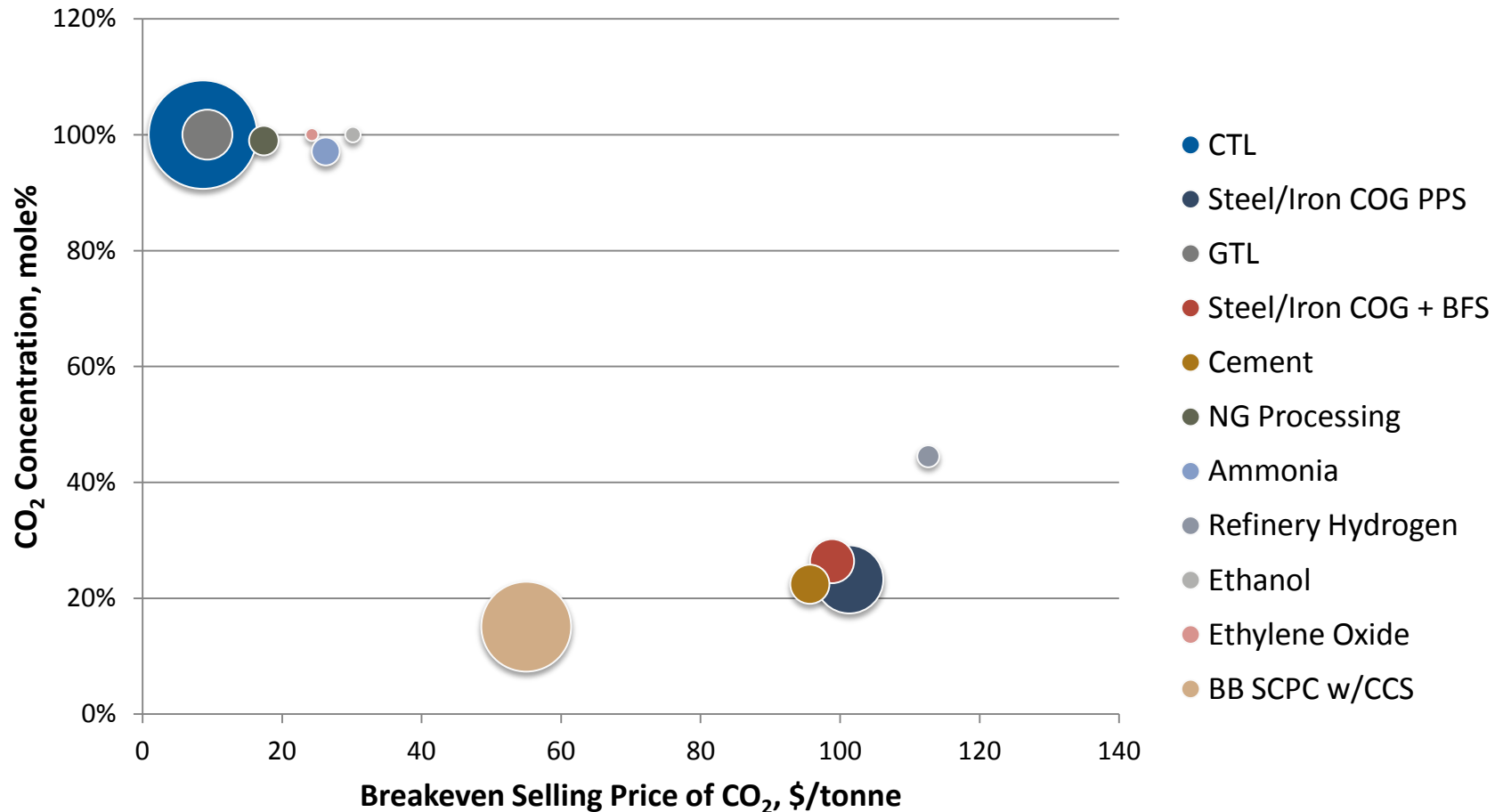
- **Many different parameters of the base plants have an effect on the breakeven selling price of CO₂. The following have the greatest effect:**
 - Concentration of CO₂ in the exhaust stream
 - Being able to meet CO₂ pipeline specifications without separation of the CO₂ greatly drives down the cost
 - Scale of the plant
 - Scale economies reduce specific capital costs

Results

	Capture Stream CO ₂ Concentration (mole %)	Captured CO ₂ (tonne/yr)*	Greenfield Breakeven Cost (\$/tonne CO ₂)	Retrofit Breakeven Cost (\$/tonne CO ₂)
Coal-to-Liquids	100.00	8,743,323	8.66	N/A
Gas-to-Liquids	100.00	1,858,767	9.29	N/A
Natural Gas Processing	99.00	649,198	17.38	17.56
Ethylene Oxide	100.00	121,501	24.28	24.52
Ammonia	97.10	458,400	26.26	26.52
Ethanol	100.00	143,045	30.15	30.46
Cement	22.40	1,140,697	95.66	100.44
Steel/Iron COG + BFS	23.23	2,754,966	N/A	98.84
Steel/Iron COG PPS	26.42	1,155,413	N/A	101.31
Refinery Hydrogen	44.52	273,860	112.64	118.27
BB SCPC w/CCS	15.1%	4,807,429	60	65 - 70

*100% CF assumed
BB SCPC uses utility finance structure

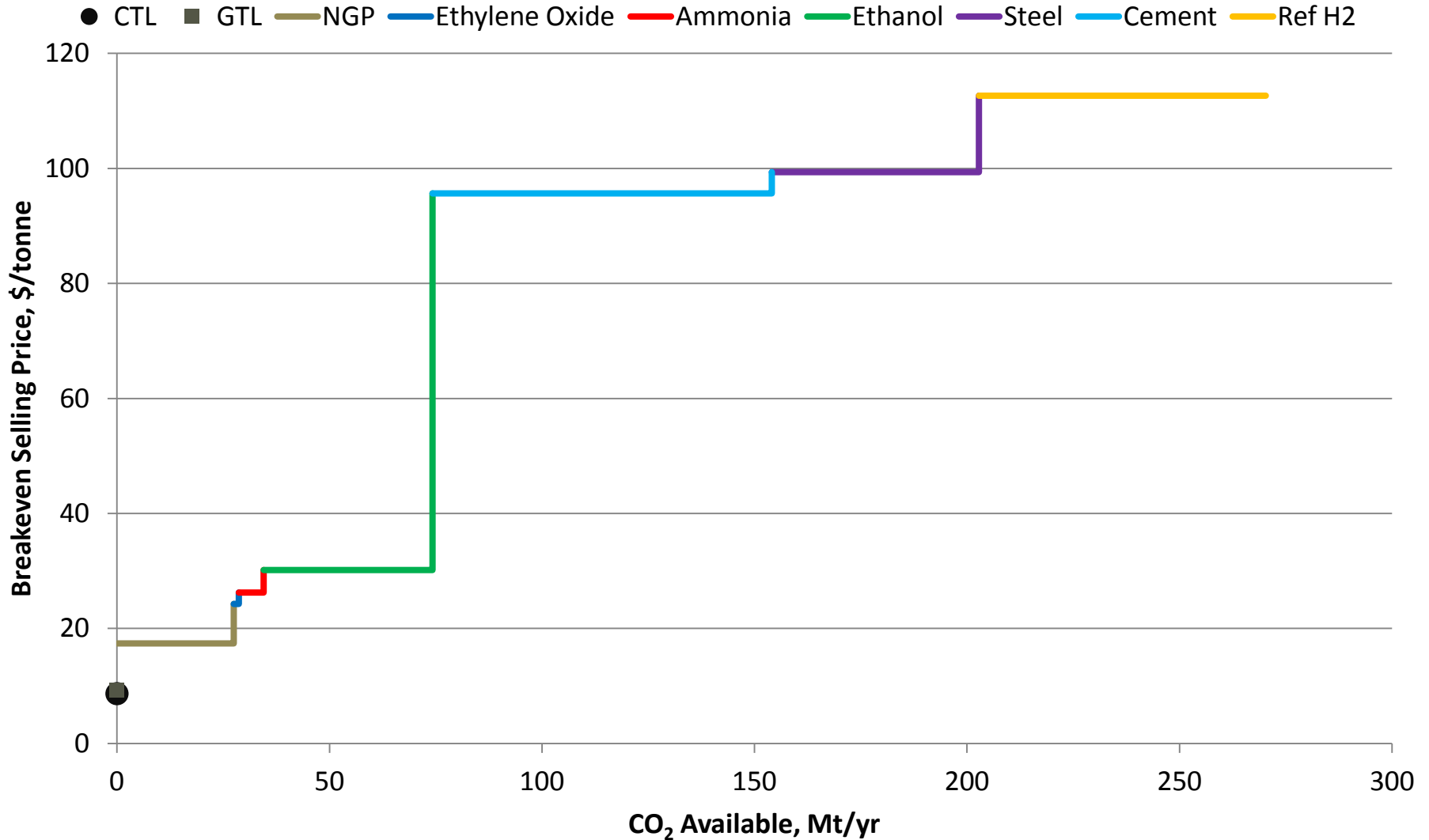
Results



- Size of circle Illustrates relative quantity of CO₂ being captured on a plant basis

Incremental CO₂ Supply versus Breakeven Selling Price

Based on Greenfield Prices except for Steel Process



Sensitivities

Sensitivities

Cement

- **Plant – 992,500 tonne/year**
- **Feed Stock – Various**
- **Point Source**
 - Kiln Off-gas
 - 22.4% CO₂
 - Partial Pressure: 3.29 psia
 - Kiln off-gas may have higher than acceptable levels of SO_x/No_x requiring addition of selective catalytic reduction (SCR) and flue gas desulfurization (FGD).
 - A sensitivity to this case was performed, and the results show that the addition of SCR and FGD has the potential to add \$26.43/tonne to the retrofit costs.

Sensitivities

Cement Continued

	Cement	Purity Sensitivity
	\$/tonne CO ₂	\$/tonne CO ₂
Capital Charges	32.89	45.33
Fixed O&M	9.99	13.76
Variable O&M	14.99	20.64
Consumables	2.54	5.41
Purchased Power	9.45	9.90
Purchased Natural Gas	25.80	25.80
Total Breakeven Cost	95.66	120.83

Sensitivities

- **Financing assumptions**
 - A 10-yr economic life of the project increases break even CO₂ price by 16-20% compared to the assumed 30-yr economic life
- **Price of power from the grid**
 - Purchased power makes up 25% of break even cost for high CO₂ purity sources
 - Breakeven cost for low CO₂ purity sources increases more rapidly with increasing COE due to higher auxiliary loads
- **Price of natural gas for thermal loads**
 - Purchased natural gas makes up ~25% of break-even cost for low CO₂ purity sources
- **CO₂ stream purity**
 - Only assessed for cases requiring CO₂ separation (low CO₂ purity sources)
- **Plant size in terms of CO₂ emissions per year**
 - Typically varied over the range of operating US plants
- **Retrofit factor**

Questions?



High CO₂ Concentration Sources

Process	Capture Stream CO ₂ Concentration (mole %)	Partial Pressure (psia)	Captured CO ₂ (tonne/yr)
Coal-to-Liquids	100.0%	265	8,743,323
Gas-to-Liquids	100.0%	265	1,858,767
Ethanol	100.0%	18.40	143,045
Ethylene Oxide	100.0%	43.50	121,501
Natural Gas Processing	99.0%	23.27	649,198
Ammonia	97.1%	22.82	458,400

- Assumed that high CO₂ concentration vent streams can meet CO₂ pipeline specs* through compression and cooling alone (e.g. ≥ 95% CO₂)
- Note: 4.8 Mt CO₂/year assumed to be captured in a 550 MW SCPC with CCS

Lower CO₂ Concentration Sources

Process	Capture Stream CO ₂ Concentration (mole %)	Partial Pressure (psia)	Captured CO ₂ (tonne/yr)
Refinery Hydrogen	44.5%	8.90	273,860
Steel/Iron COG + BFS	26.4%	3.88	1,155,413
Steel/Iron COG PPS	23.2%	3.41	2,754,966
Cement	22.4%	3.29	1,140,697

- Assumed that lower CO₂ concentration vent streams will need to be equipped with both CO₂ capture and compression equipment to meet CO₂ pipeline specs (e.g. ≥ 95% CO₂)
- Note: 4.8 Mt CO₂/year assumed to be captured in a 550 MW SCPC with CCS

Equipment Modeled

Compression

- **Quotes for two types of compressor were obtained**
 - Centrifugal compression was used for relatively high CO₂ flowrates
 - Reciprocating compression was used for low CO₂ flowrates
 - 615,900 tonnes CO₂/yr (678,900 tons CO₂/yr).

Separation

- **MDEA AGR unit with a packaged boiler to regenerate the MDEA**
 - Produces CO₂ at 19.7 psia
 - Assumes 95% capture (of CO₂ in treated stream)

Capacity Factor – 85% for all cases

CO₂ Impurity Design Parameters

Component	Unit (Max unless Otherwise noted)	Carbon Steel Pipeline		Enhanced Oil Recovery		Saline Reservoir Sequestration		Saline Reservoir CO ₂ & H ₂ S Co-sequestration		Venting Concerns (See Section 3.0)
		Conceptual Design	Range in Literature	Conceptual Design	Range in Literature	Conceptual Design	Range in Literature	Conceptual Design	Range in Literature	
CO ₂	vol% (Min)	95	90-99.8	95	90-99.8	95	90-99.8	95	20 – 99.8	Yes-IDLH 40,000 ppmv
H ₂ O	ppm _{wf}	300	20 - 650	300	20 - 650	300	20 - 650	300	20 - 650	
N ₂	vol%	4	0.01 - 7	1	0.01 - 2	4	0.01 - 7	4	0.01 – 7	
O ₂	vol%	4	0.01 – 4	0.01	0.001 – 1.3	4	0.01 – 4	4	0.01 – 4	
Ar	vol%	4	0.01 – 4	1	0.01 – 1	4	0.01 – 4	4	0.01 – 4	
CH ₄	vol%	4	0.01 – 4	1	0.01 – 2	4	0.01 – 4	4	0.01 – 4	Yes-Asphyxiate, Explosive
H ₂	vol%	4	0.01 - 4	1	0.01 – 1	4	0.01 – 4	4	0.02 – 4	Yes-Asphyxiate, Explosive
CO	ppm _v	35	10 - 5000	35	10 - 5000	35	10 - 5000	35	10 - 5000	Yes-IDLH 1,200 ppmv
H ₂ S	vol%	0.01	0.002 – 1.3	0.01	0.002 – 1.3	0.01	0.002 – 1.3	75	10 - 77	Yes-IDLH 100 ppmv
SO ₂	ppm _v	100	10 - 50000	100	10 - 50000	100	10 - 50000	100	10 - 50000	Yes-IDLH 100 ppmv
NO _x	ppm _v	100	20 - 2500	100	20 - 2500	100	20 - 2500	100	20 - 2500	Yes-IDLH NO-100 ppmv, NO ₂ - 200 ppmv

CO₂ Impurity Design Parameters cont.

Component	Unit (Max unless Otherwise noted)	Carbon Steel Pipeline		Enhanced Oil Recovery		Saline Reservoir Sequestration		Saline Reservoir CO ₂ & H ₂ S Co-sequestration		Venting Concerns (See Section 3.0)
		Conceptual Design	Range in Literature	Conceptual Design	Range in Literature	Conceptual Design	Range in Literature	Conceptual Design	Range in Literature	
NH ₃	ppm _v	50	0 - 50	50	0 - 50	50	0 - 50	50	0 - 50	Yes-IDLH 300 ppmv
COS	ppm _v	trace	trace	5	0 - 5	trace	trace	trace	trace	Lethal @ High Concentrations (>1,000 ppmv)
C ₂ H ₆	vol%	1	0 - 1	1	0 - 1	1	0 - 1	1	0 - 1	Yes-Asphyxiant, Explosive
C ₃ +	vol%	<1	0 - 1	<1	0 - 1	<1	0 - 1	<1	0 - 1	
Part.	ppm _v	1	0 - 1	1	0 - 1	1	0 - 1	1	0 - 1	
HCl	ppm _v	N.I.*	N.I.*	N.I.*	N.I.*	N.I.*	N.I.*	N.I.*	N.I.*	Yes-IDLH 50 ppmv
HF	ppm _v	N.I.*	N.I.*	N.I.*	N.I.*	N.I.*	N.I.*	N.I.*	N.I.*	Yes-IDLH 30 ppmv
HCN	ppm _v	trace	trace	trace	trace	trace	trace	trace	trace	Yes-IDLH 50 ppmv
Hg	ppm _v	N.I.*	N.I.*	N.I.*	N.I.*	N.I.*	N.I.*	N.I.*	N.I.*	Yes-IDLH 2 mg/m ³ (organo)
Glycol	ppb _v	46	0 - 174	46	0 - 174	46	0 - 174	46	0 - 174	
MEA	ppm _v	N.I.*	N.I.*	N.I.*	N.I.*	N.I.*	N.I.*	N.I.*	N.I.*	MSDS Exp. Limits 3 ppmv ₃ 6 mg/m ³
Selexol	ppm _v	N.I.*	N.I.*	N.I.*	N.I.*	N.I.*	N.I.*	N.I.*	N.I.*	

Retrofit Assumptions

- **High Concentration Sources**

- Retrofit factors deviate from recommendations in NETL’s “Retrofit Cost Analysis for Post-combustion CO₂ Capture” due to:
 - Do not use an amine solvent-based CO₂ separation system
 - These industrial sources tend to be significantly smaller than the utility scale power plants for which these factors were developed

- **Low Concentration Sources**

- Retrofit factors align with recommendations in NETL’s “Retrofit Cost Analysis for Post-combustion CO₂ Capture” even though:
 - CO₂ separation is performed using MDEA system, rather than MEA system
 - These industrial sources tend to be significantly smaller than the utility scale power plants for which these factors were developed

Industrial Processes – High Purity Sources

Ethanol Process

- **Plant – 50 million gallon/year of Ethanol utilizing dry mill process**
- **Feedstock– Corn**
- **Point Source**
 - Fermentation off gas stream
 - 100% pure CO₂
 - Partial Pressure: 18.40 psia

Ethanol Breakeven Cost Breakout	
	\$/tonne CO ₂
Capital Charges	12.20
Fixed O&M	4.30
Variable O&M	6.46
Consumables	0.38
Purchased Power	6.82
Purchased Natural Gas	0.00
Total Breakeven Cost	30.15

Ammonia Process

- **Plant – 907,000 tonnes/year of Ammonia**
 - 28% of total CO₂ produced is used to make Urea
 - 38% of total CO₂ produced available for EOR
- **Feed Stock – Natural Gas**
- **Point Source**
 - CO₂ Stripper Vent
 - 97.1% CO₂
 - Partial Pressure: 22.82 psia

Ammonia Breakeven Cost Breakout	
	\$/tonne CO ₂
Capital Charges	10.44
Fixed O&M	3.69
Variable O&M	5.54
Consumables	0.20
Purchased Power	6.38
Purchased Natural Gas	0.00
Total Breakeven Cost	26.26

Ethylene Oxide

- **Plant – 364,500 tonnes/year**
 - Rectisol unit assumed to be used in the plant
- **Feed Stock – Ethylene**
- **Point Source**
 - AGR unit CO₂ stream
 - 100% CO₂
 - Partial Pressure: 43.50 psia

Ethylene Breakeven Cost Breakout	
	\$/tonne CO ₂
Capital Charges	9.85
Fixed O&M	3.47
Variable O&M	5.20
Consumables	0.27
Purchased Power	5.49
Purchased Natural Gas	0.00
Total Breakeven Cost	24.28

Natural Gas Processing

- **Plant – 500 MMscf/day**
- **Feed Stock – Raw Natural Gas**
 - Can contain 2 to 70 % by volume CO₂
 - Assumed Michigan Basin producing formation containing 10.2 mole percent CO₂
- **Point Source**
 - CO₂ vent
 - 99% CO₂
 - Partial Pressure: 23.27 psia

Natural Gas Breakeven Cost Breakout	
	\$/tonne CO ₂
Capital Charges	6.14
Fixed O&M	2.17
Variable O&M	3.25
Consumables	0.13
Purchased Power	5.69
Purchased Natural Gas	0.00
Total Breakeven Cost	17.38

Coal-to-Liquids

- **Plant – 50,000 bbl/day of Liquids**
- **Feed Stock – Coal**
- **Point Source**
 - AGR unit CO₂ stream
 - 100% CO₂
 - Partial Pressure: 265 psia

CTL Breakeven Cost Breakout	
	\$/tonne CO ₂
Capital Charges	3.11
Fixed O&M	1.10
Variable O&M	1.65
Consumables	0.14
Purchased Power	2.65
Purchased Natural Gas	0.00
Total Breakeven Cost	8.66

Gas-to-Liquids

- **Plant – 50,000 bbl/day of Liquids**
- **Feed Stock – Natural Gas**
- **Point Source**
 - AGR unit CO₂ stream
 - 100% CO₂
 - Partial Pressure: 265 psia

GTL Breakeven Cost Breakout	
	\$/tonne CO ₂
Capital Charges	3.83
Fixed O&M	1.35
Variable O&M	2.03
Consumables	0.14
Purchased Power	1.93
Purchased Natural Gas	0.00
Total Breakeven Cost	9.29

Industrial Processes – Lower Purity Sources

Refinery Hydrogen

- **Plant – 59,000 tonnes/year Hydrogen production**
- **Feed Stock – Natural gas and refinery off gas**
- **Point Source**
 - PSA tail gas
 - 44.5% CO₂
 - Partial Pressure: 8.90 psia

Refinery Hydrogen Breakeven Cost Breakout	
	\$/tonne CO ₂
Capital Charges	41.37
Fixed O&M	12.57
Variable O&M	18.86
Consumables	2.71
Purchased Power	11.24
Purchased Natural Gas	25.88
Total Breakeven Cost	112.64

Steel/Iron Process

- **Plant – 2.54 million tonnes/year from BOF plant**
 - Arc Furnace produces much less CO₂ per pound of steel
- **Feed Stock – 75% raw material, 25% recycled steel**
- **Point Sources**
 - Coke oven gas (COG) power stack (PPS)
 - Blast furnace stove (BFS) PPS could have also been used
 - 23.2% CO₂
 - Partial Pressure: 3.41 psia
 - COG+ BFS combined
 - 26.4% CO₂
 - Partial Pressure: 3.88 psia

Steel/Iron Process Continued

Steel/ Iron Breakeven Cost Breakout \$/tonne CO ₂			
	Combined	Steel/Iron COG + BFS	Steel/Iron COG PPS
Capital Charges	33.66	34.48	33.49
Fixed O&M	10.23	10.47	10.17
Variable O&M	15.34	15.71	15.26
Consumables	2.67	2.67	2.67
Purchased Power	10.20	10.26	10.17
Purchased Natural Gas	27.27	27.72	27.08
Total Breakeven Cost	99.36	101.31	98.84

Sensitivities

Cement

- **Plant – 992,500 tonne/year**
- **Feed Stock – Various**
- **Point Source**
 - Kiln Off-gas
 - 22.4% CO₂
 - Partial Pressure: 3.29 psia
 - Kiln off-gas may have higher than acceptable levels of SO_x/No_x requiring addition of selective catalytic reduction (SCR) and flue gas desulfurization (FGD).
 - A sensitivity to this case was performed, and the results show that the addition of SCR and FGD has the potential to add \$26.43/tonne to the retrofit costs.

Sensitivities

Cement Continued

	Cement	Purity Sensitivity
	\$/tonne CO ₂	\$/tonne CO ₂
Capital Charges	32.89	45.33
Fixed O&M	9.99	13.76
Variable O&M	14.99	20.64
Consumables	2.54	5.41
Purchased Power	9.45	9.90
Purchased Natural Gas	25.80	25.80
Total Breakeven Cost	95.66	120.83